

6-V to 30-V Input, 3-A Output, Synchronous Step-Down DC-DC Converter

GENERAL DESCRIPTION

The NS3003 is a High Efficiency Synchronous DCDC Buck Converters with CV / CC modes, which can output to 3A in a wide input range from 6 V to 30 V. The NS3003 operates either in CV (Constant Voltage) mode or CC (Constant Current) mode. The output voltage can be programed through the FB pin respectively. In order to achieve better EMI performance, the switching frequency was fixed at 165 kHz. NS3003 is available in SOP8-EP package which is beneficial for compact solution as well as thermal dissipation.

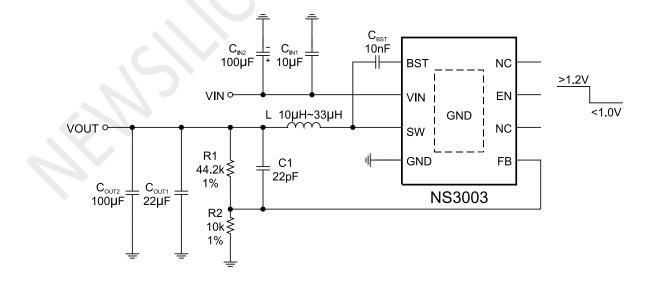
FEATURES

- Wide Input Voltage Range: 6V ~ 30V
- Low R_{DS(ON)} for Internal Switches (Top/Bottom): 90mΩ/65 mΩ
- Up to 3A output current capability
- Up to 95 % Efficiency
- 165kHz Switching Frequency Minimize the External Components
- Internal 1.5-ms Soft-Start
- Input Under Voltage Lockout
- Input Over Voltage Protection
- Cycle by Cycle Peak Current Limit
- Thermal Shutdown
- Thermally Enhanced SOP8-EP Package

APPLICATION

- Automotive Systems
- Printer Systems
- Industrial Power Systems
- Distributed Power Systems
- Network Terminal Equipment

TYPICAL APPLICATIONS



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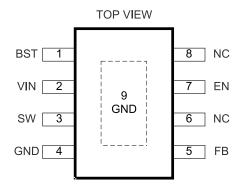
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PIN CONFIGURATION



PIN DESCRIPTIONS

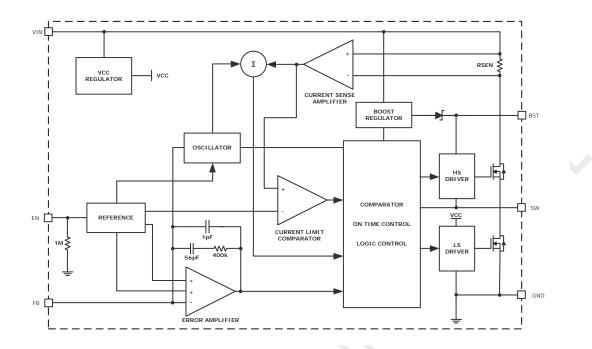
PIN	NAME	DESCRIPTION
1	BST	Boot-Strap Pin. Supply high side gate driver. Decouple this pin to SW pin with10nF
I		ceramic cap.
2	VIN	Supply Voltage. The NS3003 operates from a 6V to 30V input rail. Requires C _{IN} to
Z		decouple the input rail. Connect using a wide PCB trace.
3	SW	Switch Output. Connect using a wide PCB trace.
4	GND	System Ground. Reference ground of the regulated output voltage: requires extra
4		care during PCB layout. Connect to GND with copper traces and vias.
5	FB	Output Feedback Pin. Connect this pin to the center point of the output resistor
5		divider to program the output voltage
6	NC	NC
7	EN	Pull High to enable the NS3003. For automatic start-up, connect EN to IN using a
/		resistor. Do not float.
8	NC	NC
9	GND	EPAD, connect to GND





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SYSTEM BLOCK DIAGRAM



ABSOLUTE MAXIMUM RATINGS

PARAMETER	MIN	MAX	UNIT
Supply Input Voltage	-0.3	38	V
SW,EN Voltage	-0.3	V _{IN} + 0.3	V
FB, BS-SW Voltage	-0.3	4	V
Junction Temperature Range	-40	150	°C
Lead Temperature (Soldering, 10 sec.)		260	°C
Storage Temperature Range	-65	150	°C
Dynamic SW Voltage in 10ns Duration	GND-5V	V _{IN} +3V	V
Package Thermal Resistance θ_{JA}		42.1	°C/W
Package Thermal Resistance θ_{JC}		50.9	°C/W
HBM(Human Body Mode)		2	kV
MM(Machine Mode)		200	V



ESD(electrostatic discharge) sensitive device.

Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

RECOMMENDED OPERATING CONDITIONS

PARAMETER	MIN	MAX	UNIT
Supply Input Voltage	6	30	V
Junction Temperature Range	-40	150	°C
Ambient Temperature Range	-40	85	°C







ELECTRICAL CHARACTERISTICS

$(V_{IN} = 12V, V_{OUT} = 5V)$	1 10.11 C 14		1	······································
$(V_{1}) = 1/V_{2} V_{01T} = 5V_{1}$	I = I()IIH (aut = 44	$11E I_{A} = 75^{2}(I_{A}) = 10^{12}$	- ΤΑ ΠΠΑςς Ατηρηγ	MICA CHACITIAN
$(v_{IN} - 12v, v_{OII} - 3v,$				

	TEST CONDITIONS	MIN	TYP	MAX	UNIT
V _{IN}		6		30	V
V _{OVP}				30	V
V _{HYS}			3		V
VUVP				5.3	V
V _{HYS}			0.6		V
lq	I _{OUT} =0,V _{FB} =V _{REF} ×105%		110		μΑ
I _{SHDN}	$V_{EN} = 0$		2		μΑ
$V_{\text{EN}_{R}}$			1.2		V
$V_{\text{EN}_{\text{F}}}$			1		V
V _{REF}			0.925		V
I _{FB}	V _{FB} =3.3V	-50		50	nA
R _{DSON}			90		mΩ
R _{DSON}			65		mΩ
			50		ns
			100		ns
T _{ON_DLY}	from EN high to SW start switching		180		μs
T _{ss}	Vout from 0 to 100%		1.5		ms
Fsw	V _{OUT} =3.3V, CCM		165		kHz
I _{LIM_TOP}			3.7		Α
I _{LIM_BOT}			3.7		Α
Т.,			150		°C
I SD			130		C
T _{HYS}	Duty = 30%		15		°C
	VHYS VUVP VHYS IQ ISHDN VEN_R VEN_F VREF IFB RDSON TON_MIN TOFF_MIN TON_DLY Tss Fsw ILM_TOP	$\begin{tabular}{ c c c c c } \hline V_{HYS} & & & & & & & \\ \hline V_{UVP} & & & & & & & \\ \hline V_{HYS} & & & & & & \\ \hline I_Q & I_{OUT}=0, V_{FB}=V_{REF}\times105\% \\ \hline I_{SHDN} & V_{EN}=0 & & & \\ \hline V_{EN_R} & & & & & \\ \hline V_{EN_R} & & & & & \\ \hline V_{EN_F} & & & & & \\ \hline V_{REF} & & & & & \\ \hline I_{FB} & V_{FB}=3.3V & & & \\ \hline R_{DSON} & & & & & \\ \hline T_{ON_MIN} & & & & \\ \hline T_{ON_DLY} & from EN high to SW \\ start switching & \\ \hline T_{SS} & V_{OUT} from 0 to 100\% \\ \hline F_{SW} & V_{OUT}=3.3V, CCM \\ \hline I_{LIM_TOP} & & \\ \hline I_{LIM_BOT} & & \\ \hline T_{SD} & & & \\ \hline \end{tabular}$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $

FUNCTIONAL DESCRIPTION

NS3003 is a high efficiency, 165kHz synchronous step-down DC/DC regulator with CV / CC modes. It utilizes internal MOSFETs to achieve high efficiency and up to 3.7 A output current in a wide input range from 6 V to 30 V. NS3003 provides protection functions such as cycle by cycle current limiting and thermal shutdown protection.

Soft Start

NS3003 has an internal soft-start circuit that limits the in-rush current during startup. This allows the converters to gradually reach the steady-state operating point, thus reducing startup stresses and surges. During startup, the switch current limit is increased in steps. The typical soft-start time is 1.5ms.

Cycle by Cycle Peak Current Limit

The peak current limit prevents the NS3003 from high inductor current and from drawing excessive current from the input voltage rail. Excessive current might occur with a shorted or saturated inductor or a heavy load or shorted output circuit condition. If the inductor current reaches the peak limit threshold, the high-side MOSFET is turned off and the low-side MOSFET is turned on to ramp down the inductor current.

Input Under-voltage Lockout(UVLO)

An input UVLO circuit prevents the converter from starting the operation until the input voltage rises above the typical UVLO threshold of 5.9 V.

A hysteresis of 600 mV is added so that the device cannot be disabled again until the input voltage drops below 5.3 V. This function is implemented in order to prevent malfunctioning of the device when the input voltage is between 5.3 V and 5.9 V.

Input Over Voltage Protection(OVP)

The input OVP is an additional function to protect the device from damage in a condition which is above the specified input voltage range. Once the input voltage is raising above input OVP threshold, 30 V typically, the NS3003 stops switching to reduce the chance of damage by the voltage spike at SW pin. The device goes back to normal operation until the input voltage falls a hysteresis about 3 V below the input OVP threshold.



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Detailed Design Procedure

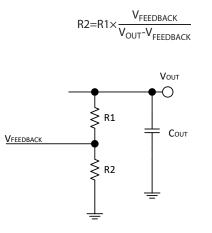
Adjusting the Output Voltage

A resistor divider from the output node to the feedback pin sets the output voltage. Recommend using 1% tolerance or better divider resistors. Start with fixed value for the R1 resistor and use Equation to calculate R2.

To improve efficiency at light loads, consider using larger-value resistors. If the values are too high, the regulator is more susceptible to noise, and voltage errors from the feedback input current are noticeable.

$$V_{OUT} = V_{FEEDBACK} \times \frac{R1 + R2}{R2}$$

Select R1 value then



Inductor Selection

Use a inductor with a DC current rating of at least 25% percent higher than the maximum load current for most applications. For highest efficiency, select an inductor with a DC resistance less than 15m Ω . For most designs, derive the inductance value from the following equation.

$$L = \frac{V_{OUT} \times (V_{IN} - V_{OUT})}{V_{IN} \times \Delta I_L \times F_S}$$

Where ΔI_L is the inductor ripple current. Choose an inductor current approximately 30% of the maximum load current. The maximum inductor peak current is:

$$I_{L(MAX)} = I_{LOAD} + \frac{\Delta I_{L}}{2}$$

Under light-load conditions (below 100mA), use a larger inductor to improve efficiency.

Input Capacitor Selection

The input current to the step-down converter is discontinuous, and therefore requires a capacitor to both supply the AC current to the step-down

converter and maintain the DC input voltage. For the best performance, use low ESR capacitors, such as ceramic capacitors with X5R or X7R dielectrics and small temperature coefficients. A 10µF capacitor is sufficient for most applications. The input capacitor requires an adequate ripple current rating because it absorbs the input switching. Estimate the RMS current in the input capacitor with:

$$I_{CIN} = I_{LOAD} \times \frac{\sqrt{V_{OUT} \times (V_{IN} - V_{OUT})}}{V_{IN}}$$

The worst-case condition occurs at $V_{\text{IN}}=2V_{\text{OUT}},$ where:



For simplification, choose an input capacitor with an RMS current rating greater than half the maximum load current. The input capacitor can be electrolytic, tantalum, or ceramic. Place a small, high-quality, ceramic capacitor $(0.1\mu F)$ as close to the IC as possible when using electrolytic or tantalum capacitors. When using ceramic capacitors, make sure that they have enough capacitance to provide sufficient charge to prevent excessive input voltage ripple. Estimate the input voltage ripple caused by the capacitance with:

$$\Delta V_{\rm IN} = \frac{I_{\rm LOAD}}{F_{\rm S} \times C_{\rm IN}} \times \frac{V_{\rm OUT}}{V_{\rm IN}} \times (1 - \frac{V_{\rm OUT}}{V_{\rm IN}})$$

Output Capacitor Selection

The output capacitor maintains the DC output voltage. Use ceramic, tantalum, or low-ESR electrolytic capacitors. Use low ESR capacitors to limit the output voltage ripple. Estimate the output voltage ripple with:

$$\Delta V_{OUT} = \frac{V_{OUT}}{F_{S} \times L} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right) \times \left(R_{ESR} + \frac{1}{8 \times F_{S} \times C_{OUT}}\right)$$

Where L is the inductor value and RESR is the equivalent series resistance (ESR) of the output capacitor.

For ceramic capacitors, the capacitance dominates the impedance at the switching frequency and causes most of the output voltage ripple. For simplification, estimate the output voltage ripple with:

$$\Delta V_{OUT} = \frac{V_{OUT}}{8 \times F_{S}^{2} \times L \times C_{OUT}} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right)$$

For tantalum or electrolytic capacitors, the ESR dominates the impedance at the switching



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frequency. For simplification, the output ripple can be approximated with:

$$\Delta V_{OUT} \!\!=\!\! \frac{V_{OUT}}{F_S \!\!\times\! L} \!\times\! \left(1 \!\!-\! \frac{V_{OUT}}{V_{IN}}\right) \!\times\! R_{ESR}$$

The characteristics of the output capacitor also affect the stability of the regulation system. The NS3003 can be optimized for a wide range of capacitance and ESR values.

For the best performance, it is recommended to use X5R or a better grade ceramic capacitor with 16V rating and more than 44μ F capacitance.

Bootstrap Capacitor Selection

Connect a 10nF ceramic capacitor between the SW and BS pins for proper operation. Recommend using a ceramic capacitor with X5R or better-grade dielectric. The capacitor should have a 6.3V or higher voltage rating.

Layout Guidelines

PC board layout is an important part of DC-DC converter design. Poor board layout can disrupt the performance of a DC-DC converter and surrounding circuitry by contributing to EMI, ground bounce, and resistive voltage loss in the traces. These can send erroneous signals to the DC-DC converter resulting in poor regulation or instability. Good layout can be implemented by following a few simple design rules.

1. Minimize area of switched current loops. In a buck regulator there are two loops where currents are switched rapidly. The first loop starts from the CIN input capacitor, to the regulator V_{IN} terminal, to the regulator SW terminal, to the inductor then out to the output capacitor C_{OUT} and load. The second loop starts from the output capacitor ground, to the regulator GND terminals, to the inductor and then

out to C_{OUT} and the load. To minimize both loop areas the input capacitor should be placed as close as possible to the V_{IN} terminal. Grounding for both the input and output capacitors should consist of a small localized top side plane that connects to GND. The inductor should be placed as close as possible to the SW pin and output capacitor.

2. Minimize the copper area of the switch node. The SW terminals should be directly connected with a trace that runs on top side directly to the inductor. To minimize IR losses this trace should be as short as possible and with a sufficient width. However, a trace that is wider than 100 mils will increase the copper area and cause too much capacitive loading on the SW terminal. The inductors should be placed as close as possible to the SW terminals to further minimize the copper area of the switch node.

3. Have a single point ground for all device analog grounds. The ground connections for the feedback components should be connected together then routed to the GND pin of the device. This prevents any switched or load currents from flowing in the analog ground plane. If not properly handled, poor grounding can result in degraded load regulation or erratic switching behavior.

4. Minimize trace length to the FB terminal. The feedback trace should be routed away from the SW pin and inductor to avoid contaminating the feedback signal with switch noise.

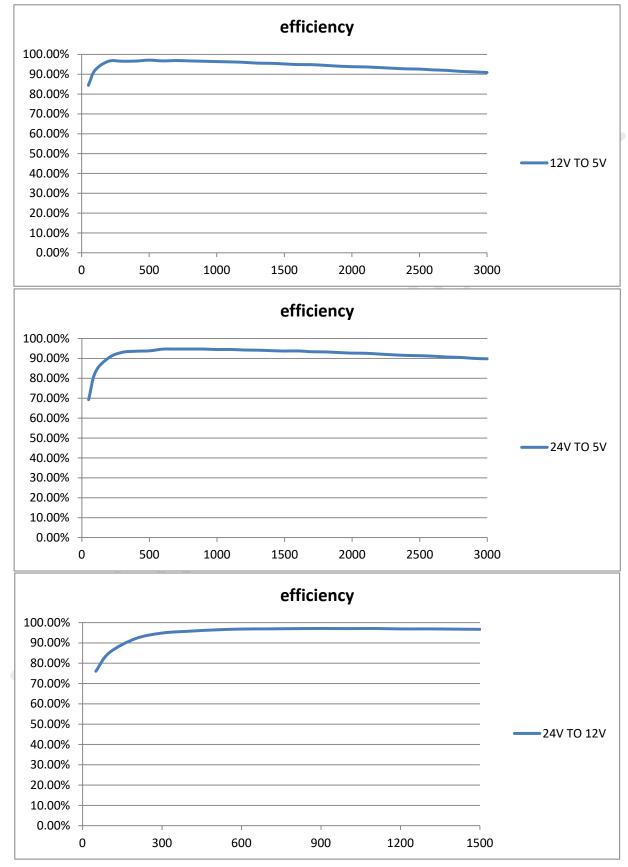
5. Make input and output bus connections as wide as possible. This reduces any voltage drops on the input or output of the converter and can improve efficiency. If voltage accuracy at the load is important make sure feedback voltage sense is made at the load. Doing so will correct for voltage drops at the load and provide the best output accuracy.





Typical Performance Characteristics

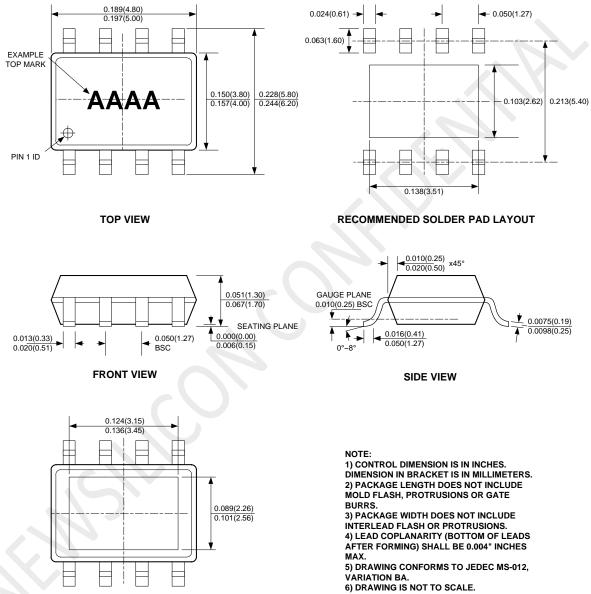
All curves taken at VIN = 12 V and 24V, VOUT = 5 V and 12V with configuration in Typical Application Circuit. $T_A = 25$ °C, unless otherwise specified.







PACKAGE



SOP8(EXPOSED PAD)



BOTTOM VIEW